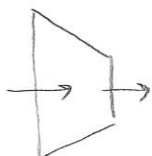


Lecture 35 - supplemental

A. Proof of  $Ma=1$  limit in converging nozzle.



The mass flow rate is a constant.

$$w = \rho A v$$

In incompressible flow  $\rho$  is a constant too, so when  $A$  decreases,  $v$  must increase. In compressible flow  $\rho$  can change. This puts a "speed limit" on  $v$ .

Proof

$$w = \rho A v$$

$$\ln w = \ln \rho + \ln A + \ln v$$

$$d(\ln w) = 0 = \frac{d\rho}{\rho} + \frac{dA}{A} + \frac{dv}{v}$$

$$-\frac{dv}{v} = \frac{d\rho}{\rho} + \frac{dA}{A} \quad (1)$$

\* Bernoulli's equation (isentropic = no friction)

$$\frac{dP}{\rho} + \frac{1}{2} d(v^2) = 0$$

$$\uparrow d(v^2) = 2v dv$$

$$\frac{dP}{\rho} + v dv = 0 \Rightarrow -v dv = \frac{dP}{\rho} \quad (2)$$

\* Equation of state for  $p$ :  $p = p(P, S)$

$$dp = \left(\frac{\partial p}{\partial P}\right)_S dP + \underbrace{\left(\frac{\partial p}{\partial S}\right)_P}_{ds=0, \text{ isentropic}} dS$$

$$dp = \underbrace{\left(\frac{dp}{dP}\right)_S}_{\frac{1}{c^2}} dP \Rightarrow dP = c^2 dp \quad (3)$$

$\frac{1}{c^2} \Rightarrow$  definition of speed of sound

\* Combine (2) & (3)

$$\frac{c^2 dp}{\rho} = -v dv$$

$$\frac{dp}{\rho} = -\frac{v^2}{c^2} \frac{dv}{v} \quad (4)$$

\* combine (1) & (4)

$$-\frac{dv}{v} = \underbrace{\frac{-v^2}{c^2}}_{Ma^2} \frac{dv}{v} + \frac{dA}{A}$$

$$\frac{dv}{v} (-1 + Ma^2) = \frac{dA}{A}$$

$$\boxed{\frac{dv}{v} = \frac{1}{Ma^2 - 1} \frac{dA}{A}}$$

\* when  $Ma = 1$ ,  $dv = 0$

\* when  $Ma < 1$ :

$dv > 0$  when  $dA < 0$   
speeds up when converging

\* when  $Ma > 1$

$dv > 0$  when  $dA > 0$   
speeds up when diverging

**B. Proof of P,T relations for compressible, isentropic flow**

(1) Mass Balance

$$\boxed{w = \rho_1 A_1 v_1} \quad (1)$$

(2) Mechanical Energy Balance

$$\frac{\Delta P}{\rho} + \frac{\Delta v^2}{2} + \cancel{g \Delta h} = \frac{1}{w} \left( \cancel{w/m} - \cancel{E_v} - E_c \right)$$

no height change
no pumps
very fast isentropic/inviscid

$$\frac{\Delta P}{\rho} + \frac{\Delta v^2}{2} = - \frac{E_c}{w} \leftarrow \text{what is } E_c?$$

$$\frac{E_c}{w} = - \frac{\Delta P}{\rho} + \int_{P_0}^{P_1} \frac{dP}{\rho}$$

↳  $\rho$  is a function of  $P$

See Dean p. 336 for derivation of  $E_c$

$$\cancel{\frac{\Delta P}{\rho}} + \frac{\Delta v^2}{2} = \cancel{\frac{\Delta P}{\rho}} - \int_{P_0}^{P_1} \frac{dP}{\rho} \Rightarrow \boxed{\int_{P_0}^{P_1} \frac{dP}{\rho} + \frac{\Delta v^2}{2} = 0} \quad (2)$$

(3) Equation of State

Assume an ideal gas:

$$\boxed{\rho = \frac{MP}{RT}} \quad (3a)$$

(see Thermodynamics textbook for more.)

$$\rightarrow c = \sqrt{\frac{\gamma RT}{M}} \quad (3b)$$

$$\rightarrow \gamma = \frac{\hat{C}_p}{\hat{C}_v} = 1.4 \quad (3c)$$

$$\rightarrow \hat{C}_p - \hat{C}_v = \frac{R}{M} \text{ or } \hat{C}_p = \frac{R}{M} \frac{\gamma}{\gamma - 1} \quad (3d)$$

(4) Total Energy Equation

$$d\left(\underbrace{u}_{\text{internal energy}} + \underbrace{\frac{v^2}{2} + \frac{P}{\rho} + gz}_{\text{mech. energy}}\right) = 0$$

$$\left\{ \begin{array}{l} d(gz) = 0 : \text{no height change} \\ H \equiv u + \frac{P}{\rho} : \text{enthalpy (definition)} \end{array} \right.$$

$$d\left(H + \frac{v^2}{2}\right) = 0 \Rightarrow dH = -\frac{1}{2} d(v^2) \quad (*)$$

$$\hat{C}_p \equiv \left. \frac{\partial H}{\partial T} \right|_p : \text{definition of heat capacity}$$

$$(**) \quad dH = \hat{C}_p dT$$

so: (\*) & (\*\*) give

$$\boxed{\hat{C}_p dT = -\frac{1}{2} d(v^2)} \quad (4)$$

Relationship for T

$$\text{Equation (4): } \hat{C}_p dT = -\frac{1}{2} d(v^2)$$

$$\hat{C}_p \Delta T = -\frac{1}{2} \Delta(v^2)$$

$$\hat{C}_p (T_1 - T_0) = -\frac{1}{2} (v_1^2 - v_0^2)$$

← let  $v_0 = 0$ , the "stagnation point" (no velocity in the tank).

$$\hat{C}_p (T_1 - T_0) = -\frac{v_1^2}{2}$$

$$\hat{C}_p \left( \frac{T_1}{T_1} - \frac{T_0}{T_1} \right) = \frac{-v_1^2}{2T_1}$$

← divide by  $T_1$ , rearrange.

$$\frac{T_0}{T_1} = \frac{v_1^2}{2\hat{C}_p T_1} + 1$$

← recall that

$$c = \sqrt{\frac{\gamma R T}{M}} \quad \text{or} \quad c^2 = \frac{\gamma R T}{M}$$

for an ideal gas.

$$\frac{T_0}{T_1} = \frac{v_1^2}{2} \frac{\gamma R}{M c_1^2} \frac{1}{\hat{C}_p} + 1$$

$$(T = \frac{M c^2}{\gamma R})$$

$$\frac{T_0}{T_1} = 1 + \frac{1}{2} \underbrace{\frac{v_1^2}{c_1^2}}_{Ma^2} \cdot \frac{\gamma R}{M \hat{C}_p} + 1$$

recall that

$$Ma = \frac{v_1}{c_1}$$

For an ideal gas:  $\hat{C}_p = \frac{R}{M} \frac{\gamma}{\gamma-1}$

$$\gamma = \frac{\hat{C}_p}{\hat{C}_v} = 1.4$$

(Equation 3d)

$$\frac{T_0}{T_1} = \frac{1}{2} Ma^2 \cdot \frac{\gamma R}{M} \cdot \frac{M}{R} \frac{\gamma-1}{\gamma} + 1$$

$$\boxed{\frac{T_0}{T_1} = 1 + \frac{\gamma-1}{2} Ma^2}$$

### Relationship for P

Equation (2):  $\int_{P_0}^{P_1} \frac{dP}{P} + \frac{\Delta v^2}{2} = 0 \rightarrow \frac{dP}{P} + \frac{1}{2} d(v^2) = 0$  (on a streamline)

• differential version

• Bernoulli's Equation!

Equation (4):  $-\frac{1}{2} d(v^2) = \hat{C}_p dT$

\* Combine:  $\frac{dP}{P} = \hat{C}_p dT$

\* Equation (3a):  $P = \frac{MP}{RT} \rightarrow \frac{dP}{(MP/RT)} = \hat{C}_p dT$

$$\frac{dP}{P} = \frac{M}{RT} \hat{C}_p dT$$

Equation (3d):  $\hat{C}_p = \frac{R}{M} \frac{\gamma}{\gamma-1}$

$$\frac{dP}{P} = \frac{M}{RT} \cdot \frac{R}{M} \frac{\gamma}{\gamma-1} dT$$

$$\frac{dP}{P} = \frac{\gamma}{\gamma-1} \frac{dT}{T} \Rightarrow \text{integrate} \Rightarrow \int_{P_0}^{P_1} \frac{dP}{P} = \frac{\gamma}{\gamma-1} \int_{T_0}^{T_1} \frac{dT}{T}$$

$$\ln P_1 - \ln P_0 = \frac{\gamma}{\gamma-1} (\ln T_1 - \ln T_0)$$

$$\ln \left( \frac{P_1}{P_0} \right) = \frac{\gamma}{\gamma-1} \ln \left( \frac{T_1}{T_0} \right) \quad \text{multiply both sides by } (-1)$$

$$\ln \left( \frac{P_0}{P_1} \right) = \frac{\gamma}{\gamma-1} \ln \left( \frac{T_0}{T_1} \right) = \ln \left( \frac{T_0}{T_1} \right)^{\frac{\gamma}{\gamma-1}} \quad \text{exponentiate both sides}$$

$$\boxed{\frac{P_0}{P_1} = \left( \frac{T_0}{T_1} \right)^{\frac{\gamma}{\gamma-1}}} \quad \text{or} \quad \boxed{\frac{T_0}{T_1} = \left( \frac{P_0}{P_1} \right)^{\frac{\gamma-1}{\gamma}}}$$

$$\boxed{\frac{P_0}{P_1} = \left[ 1 + \frac{\gamma-1}{2} Ma^2 \right]^{\frac{\gamma}{\gamma-1}}}$$

Relationship for  $\rho$ .

Equation (3a):  $\rho = \frac{MP}{RT}$ ,  $P = \frac{\rho RT}{M}$

$$\frac{P_0}{P_1} = \left( \frac{T_0}{T_1} \right)^{\frac{\gamma}{\gamma-1}} \Rightarrow \frac{\rho_0 RT_0 / M}{\rho_1 RT_1 / M} = \left( \frac{T_0}{T_1} \right)^{\frac{\gamma}{\gamma-1}}$$

$$\frac{\rho_0}{\rho_1} \cdot \frac{T_0}{T_1} = \left( \frac{T_0}{T_1} \right)^{\frac{\gamma}{\gamma-1}} \Rightarrow \frac{\rho_0}{\rho_1} = \left( \frac{T_0}{T_1} \right)^{\frac{\gamma}{\gamma-1} - 1} \quad \frac{\gamma}{\gamma-1} - \frac{\gamma-1}{\gamma-1} = \frac{1}{\gamma-1}$$

$$\boxed{\frac{\rho_0}{\rho_1} = \left( \frac{T_0}{T_1} \right)^{\frac{1}{\gamma-1}}} \quad \boxed{\frac{T_0}{T_1} = \left( \frac{\rho_0}{\rho_1} \right)^{\gamma-1}}$$

$$\boxed{\frac{\rho_0}{\rho_1} = \left[ 1 + \frac{\gamma-1}{2} Ma^2 \right]^{\frac{1}{\gamma-1}}}$$